Astronomical component estimation (ACE v.1) by time-variant sinusoidal modeling

Matthias Sinnesael, Miroslav Zivanovic, David De Vleeschouwer, Philippe Claeys, and Johan Schoukens

1 Analytical, Environmental, & Geo-Chemistry, Vrije Universiteit Brussel, 1050 Brussels, Belgium
2 Department of Electrical and Electronic Engineering, Universidad Pública de Navarra, 31006 Pamplona, Spain
3 MARUM, Center for Marine Environmental Science, Leobener Strasse, 28359 Bremen, Germany
4 Department of Fundamental Electricity and Instrumentation, Vrije Universiteit Brussel, 1050 Brussels, Belgium

Correspondence to: Matthias Sinnesael (masinnes@vub.ac.be)

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Abstract. Accurately deciphering periodic variations in paleoclimate proxy signals is essential for cyclostratigraphy. Classical spectral analysis often relies on methods based on (fast) Fourier transformation. This technique has no unique solution separating variations in amplitude and frequency. This characteristic can make it difficult to correctly interpret a proxy’s power spectrum or to accurately evaluate simultaneous changes in amplitude and frequency in evolutionary analyses. This drawback is circumvented by using a polynomial approach to estimate instantaneous amplitude and frequency in orbital components. This approach was proven useful to characterize audio signals (music and speech), which are non-stationary in nature. Paleoclimate proxy signals and audio signals share similar dynamics; the only difference is the frequency relationship between the different components. A harmonic-frequency relationship exists in audio signals, whereas this relation is non-harmonic in paleoclimate signals. However, this difference is irrelevant for the problem of separating simultaneous changes in amplitude and frequency.

Using an approach with overlapping analysis frames, the model (Astronomical Component Estimation, version 1: ACE v.1) captures time variations of an orbital component by modulating a stationary sinusoid centered at its mean frequency, with a single polynomial. Hence, the parameters that determine the model are the mean frequency of the orbital component and the polynomial coefficients. The first parameter depends on geologic interpretations, whereas the latter are estimated by means of linear least-squares. As output, the model provides the orbital component waveform, either in the depth or time domain. Uncertainty analyses of the model estimates are performed using Monte Carlo simulations. Furthermore, it allows for a unique decomposition of the signal into its instantaneous amplitude and frequency. Frequency modulation patterns reconstruct changes in accumulation rate, whereas amplitude modulation identifies eccentricity-modulated precession. The functioning of the time-variant sinusoidal model is illustrated and validated using a synthetic insolation signal. The new modeling approach is tested on two case studies: (1) a Pliocene–Pleistocene benthic δ18O record from Ocean Drilling Program (ODP) Site 846 and (2) a Danian magnetic susceptibility record from the Contessa Highway section, Gubbio, Italy.

1 Introduction

Variations in solar radiation received by the Earth are caused by quasi-periodic changes in its astronomical parameters: precession, obliquity and eccentricity. These quasi-periodic oscillations induce climate variations, which are often recorded in sedimentological archives (Hinnov, 2013). The periodicities of the different orbital cycles are reasonably well-constrained for the last 50 Myr (Berger et al., 1992; Laskar et al., 2004; 2011a, b; Westerhold et al., 2012; Waltham, 2015) and over the last 20 years, the application of astrochronology and cyclostratigraphy to numerous records throughout the Cenozoic led to significant improvements of the geological timescale (both in precision and accuracy: Hinnov and Hilgen, 2012). Moreover, the detection of an as-
Astronomical imprint in sedimentological archives sheds light on the relative contribution of orbital parameters to climate variability, and provides hints to which parts of the globe (tropical vs. high latitudes) dominantly drive global climate change.

The identification and extraction of the orbital components is essential in studies applying the astronomical theory (Muller and MacDonald, 2000). The interpretation of those components converts distance series into time series. Various techniques for distance- and time-series analysis allow for this quantitative assessment in a sedimentological archive. Spectral analysis constitutes the foundation of this process (Hinnov, 2013). A broad range of spectral analysis techniques exists. A periodogram depicts the spectral power of a signal using discrete (fast) Fourier transformations (FFT). Thomson (1982) introduced the multi-taper method (MTM) to overcome some of the limitations of conventional Fourier transformations. The MTM harmonic analyses are also applied on moving analysis frames (i.e., moving window approach) with the aim to localize principal orbital components jointly in the time and frequency domain, e.g., through evolutive harmonic analysis (Meyers et al., 2001; Pälike et al., 2006; Meyers and Hinnov, 2010). In this study the term analysis frame is preferred over the term (moving window) to avoid confusion with the window (or tapering) function terminology, which is often encountered in signal processing too. Different astrochronological studies rather use moving analysis frame FFT (e.g., Lourens and Hilgen, 1997; Martinez et al., 2012, 2015; Yao et al., 2015) or continuous wavelet transform, describing the signal through a scalogram – a bank of user-defined filters with time-varying non-uniform resolution (e.g., Torrence and Campo, 1998; De Vleeschouwer et al., 2013).

The aforementioned methods and most other commonly used in cyclostratigraphy are non-parametric in nature, which means that no assumption about the origin of the data is taken into account. Accordingly, they cannot ensure unique instantaneous amplitude–frequency description of a signal (Boashash, 1992) and therefore can hamper a correct interpretation of a proxy series, as discussed, e.g., in Meyers et al. (2001) or Laurin et al. (2016). Hiatuses, noise and changes in sedimentation rate are additional sources of uncertainty (e.g., Meyers and Sagemann, 2004; Meyers et al., 2008).

Recently, a parametric method, a.k.a. TimeOpt model, has been introduced (Meyers, 2015) that combines band-pass filtering, the Hilbert transform and specific signal modeling to describe the precession-band envelope from stratigraphic data. The signal model consists of a set of sinusoids with constant amplitudes plus noise. The model parameter (amplitudes) estimates are obtained by linear least-squares regression across a fine grid of sedimentation rates and the one providing the largest goodness-of-fit is retained. A constraint of this approach is related to the assumption that sedimentation rate is constant within the analysis frame – stratigraphic interval analyzed. For certain cases this might be approximately true; in a more general scenario, however, such an assumption will give rise to a model–data mismatch.

This study circumvents this drawback by using a polynomial modeling approach to estimate and extract instantaneous amplitude and frequency in orbital components. The approach has been proven useful to characterize audio signals (music and speech), which are non-stationary in nature (Zivanovic and Schoukens, 2011, 2012). Paleoclimate proxy signals and audio signals share similar dynamics; the only difference is the frequency relationship between the signal components. A harmonic–frequency relationship exists in audio signals, whereas this relation is non-harmonic in paleoclimate signals. By dropping the harmonicity constraint in the model for audio signals, a proxy signal is conceived as a collection of non-harmonic sinusoids, whose instantaneous amplitude and frequency vary over the record. Those variations are captured by polynomials, whose coefficients describe the relationship between varying amplitude and frequency of the sinusoids in an analysis frame. The main benefit of this approach is that short-term variations in sedimentation rate can be captured by the proposed method, as the signal model allows for instantaneous frequency change in the analysis frame. Moreover, for each data sample the sedimentation rate can be estimated leading to the concept of instantaneous sedimentation rate. The signal model identification (parameter estimation) boils down to solving a system of linear equations. Additionally, a measure for the uncertainty of the model estimates is given by means of Monte Carlo simulations.

After introducing the reader to the ACE v.1 model, distance-series analysis on a modified insolation data for the last 6 Myr as modeled by Laskar et al. (2004) is carried out. Thereafter, a first case study using an un-tuned Plioce–Pleistocene benthic oxygen isotope (δ18O) record from Ocean Drilling Program (ODP) Site 846 (Mix et al., 1995; Shackleton et al., 1995) is tested. A second case study deals with a Danian magnetic susceptibility record from the pelagic carbonate Contessa Highway section in Gubbio, Italy (Sinnesael et al., 2016).

2 Methods
2.1 Extraction of orbital waveforms

Let us consider a geologic succession that is sampled uniformly in the spatial domain at depths z1, z2 ... with z0 being the sampling interval. In an N-point measurement analysis frame, the stratigraphic record y(zn) can be represented analytically as a sum of K sinusoids – principal astronomical forcing components sk(zn) embedded in the stratigraphic data – plus stochastic perturbation e(zn):

\[ y(z_n) = \sum_{k=1}^{K} s_k(z_n) + e(z_n). \]  (1)
The components responsible for astronomically forced insolation are Earth’s orbital eccentricity, obliquity and precession, whilst the perturbation accounts for climatic and stratigraphic noise (e.g., Meyers et al., 2008). The sinusoids $s_k(z_n)$ are typically non-stationary, exhibiting some variations in the instantaneous amplitude and phase within the analysis frame:

$$y(z_n) = \sum_{k=1}^{K} A_k(z_n) \cos \left[ 2\pi f_k z_n + \phi_k(z_n) \right] + e(z_n),$$

where $f_k$ are the average spatial frequencies in cycle m$^{-1}$. The instantaneous amplitude (envelope) $A_k(z_n)$ originates in the solar system dynamics. The instantaneous phase has two components: (i) the linear phase term $2\pi f_k z_n$ determined by the corresponding orbital cycle, and (ii) phase fluctuation term $\phi_k(z_n)$, chiefly due to climate-sensitive sedimentation.

The goal is to estimate $s_k(z_n)$, $k = 1 \ldots K$ from the noisy record $y(z_n)$. Strictly speaking, the model as described in Eq. (2) cannot be solved because more parameters are present (unknowns, i.e., $A_k(z_n)$ and $\phi_k(z_n)$) than there are measurement points: assuming the frequencies $f_k$ a priori known, there are $2KN$ parameters for $N$ measurements. Although this constraint is too restrictive for the purpose of the present study, it turns out that it can be relaxed by using a concept formalized in the following assumption:

Assumption 1: in absence of unconformities, $A_k(z)$ and $\phi_k(z)$ are differentiable functions of $z$ throughout the record.

Differentiability implies continuity and this holds true for records generated by the time-continuous forcing and deposition patterns in undisturbed areas. The principal advantage of this assumption is that Eq. (2) can be reformulated such to make the signal model identifiable. By using the identity $\cos(\gamma + \delta) = \cos \gamma \cos \delta - \sin \gamma \sin \delta$, Eq. (2) can be rewritten as follows:

$$y(z_n) = \sum_{k=1}^{K} a_k(z_n) \sin (2\pi f_k z_n)$$

$$+ b_k(z_n) \cos (2\pi f_k z_n) + e(z_n),$$

with

$$a_k(z_n) = -A_k(z_n) \sin (\phi_k(z_n)),$$

$$b_k(z_n) = A_k(z_n) \cos (\phi_k(z_n)).$$

Although Eqs. (2) and (3)–(5) are formally identical, they describe the dynamics of the orbital components in a very different way. The model (Eq. 2) is highly nonlinear in the sense that the cosine is non-stationary in both amplitude and frequency. The model Eqs. (3)–(5), however, is non-stationary only in amplitude (i.e., $a_k(z_n)$ and $b_k(z_n)$), with linear argument in the sine and cosine terms. According to Assumption 1 $a_k(z)$ and $b_k(z)$ are continuous functions in $z$. Accordingly, they can be approximated by spatial polynomials of order $P$ evaluated at $z_n$:

$$a_k(z_n) = a_{k,0} + a_{k,1} z_n + \cdots + a_{k,P} z_n^P \approx a_k(z_n),$$

$$b_k(z_n) = b_{k,0} + b_{k,1} z_n + \cdots + b_{k,P} z_n^P \approx b_k(z_n).$$

The “approximately equal” symbol in the last expressions accounts for possible errors in the polynomial approximation — modeling errors. By inserting Eqs. (6)–(7) into Eq. (3) the following equation is obtained:

$$y(z_n) = \sum_{k=1}^{K} (a_{k,0} + \cdots + a_{k,P} z_n^P) \sin (2\pi f_k z_n)$$

$$+ (b_{k,0} + \cdots + b_{k,P} z_n^P) \cos (2\pi f_k z_n) + e(z_n).$$

According to the last expression, orbital components can be modeled as a stationary sine–cosine $f_k$ – basis modulated by polynomials. The benefits of such a model for analyzing stratigraphic data are

1. Both instantaneous amplitude and frequency are simultaneously and compactly characterized by a small number of polynomial coefficients.

2. The number of parameters to estimate is $2KP + 1$, which can be kept smaller than $N$ by either increasing the number of measurements or reducing the number of components to be estimated.

3. The model is linear-in-parameters and can easily be estimated by means of the linear least-squares procedure, outlined in the Appendix to this paper.

Once the model parameters (polynomial coefficients in Eq. 8) are estimated, the orbital component waveforms can be extracted from the stratigraphic data in the following way:

$$\hat{s}(z_n) = \sum_{k=1}^{K} \left( \hat{a}_{k,0} + \cdots + \hat{a}_{k,P} z_n^P \right) \sin (2\pi f_k z_n)$$

$$+ \left( \hat{b}_{k,0} + \cdots + \hat{b}_{k,P} z_n^P \right) \cos (2\pi f_k z_n),$$

where the symbol $\hat{s}$ stands for estimate. The principal blocks of the present algorithm are shown in Fig. 1.

### 2.2 Sedimentation rate estimation and time axis tuning

Once the estimate of the instantaneous frequency is provided, the sedimentation rate is obtained in a straightforward manner. In what follows, a two-step algorithm is described based on the concept of amplitude-phase decomposition in non-stationary signals (Picinbono, 1997).
2.2.1 Step 1 – instantaneous phase estimation

By combining Eqs. (3)–(5) we obtain

\[ A_k(z_n) = \sqrt{a_k^2(z_n) + b_k^2(z_n)}, \quad \phi_k(z_n) = -a \tan \left( \frac{\hat{a}_k(z_n)}{\hat{b}_k(z_n)} \right), \quad k = 1 \cdots K. \quad (10) \]

The former \( A_k(z) \) is the true instantaneous amplitude whilst the latter \( \phi_k(z_n) \) is the true instantaneous phase fluctuation of the orbital components. The estimated instantaneous phase is readily obtained by means of the previously estimated signal model:

\[ \hat{\phi}_k(z_n) = -a \tan \left( \frac{\hat{a}_k(z_n)}{\hat{b}_k(z_n)} \right), \quad k = 1 \cdots K. \quad (11) \]

2.2.2 Step 2 – instantaneous frequency estimation

By definition, the instantaneous frequency is the time derivative of the instantaneous phase (Cohen, 1995):

\[ \hat{f}_k(z_n) = f_k + \frac{1}{2\pi} \left. \frac{d\phi_k(z)}{dz} \right|_{z=z_n} = f_k + \left. \frac{d\hat{a}_k(z)}{dz} \hat{\beta}_k(z) - \frac{d\hat{b}_k(z)}{dz} \hat{a}_k(z) \right|_{z=z_n}, \quad k = 1 \cdots K. \quad (12) \]

Assuming that the sinusoids in the stratigraphic signal model are correctly associated with the astronomical forcing components, the sedimentation rate \( r_k(z_n) \) can be estimated for each component:

\[ r_k(z_n) = \frac{F_k \text{ (kyr}^{-1})}{f_k \text{ (cm}^{-1})}, \quad k = 1 \cdots K. \quad (14) \]

Recalling the definition of sedimentation rate:

\[ r(z) = \frac{dz}{dt} \quad (16) \]

the spatial–temporal conversion is carried out by reformulating Eq. (16) as a function of space and then integrating it over space. Finally, the integrals are approximated by means of partial sums:

\[ r_n = \int_0^z \frac{dz}{r(z)} \approx z_0 \sum_{j=1}^{n\cdot1} \left( r(z_j) \right)^{-1}, \quad n = 1 \cdots N. \quad (17) \]

The last expression gives the time points that mitigate the distortion of the spatial axis due to varying sedimentation rate.

2.3 Practical considerations

In the present section, the choice of analysis parameters involved with stratigraphic signal model estimation is discussed.

2.3.1 Size of the analysis frame – \( N \)

This data-dependent issue is dealt with in numerous areas of signal processing and, to the best of our knowledge, there is no analytical solution. Most approaches are heuristic; however, they are usually quite effective as long as there is some a priori knowledge about the problem at hand. Depending on the data record, a larger or shorter frame size might be appropriate but no frame size is adequate for all data.

Basically, two constraints must be considered when choosing the number of measurement points for analysis. The lower bound on \( N \) is settled by the frequency resolution (i.e., \( \frac{1}{2\pi f_k} \)) needed either to resolve closely spaced sinusoidal components (e.g., the different precession components) or to capture at least one period of the slowest signal component, e.g., long-term eccentricity (i.e., Rayleigh frequency). This piece of information is usually available beforehand.

The upper bound on \( N \) depends on the speed of fluctuations of the instantaneous amplitude and frequency along the record. Excepting for some special cases, this is something that we do not know a priori. Accordingly, a reasonable decision is to restrict the choice of \( N \) to the lower bound.

2.3.2 Selection of the components frequencies – \( f_k \)

According to Eq. (2) \( f_k \) are defined as the mean sinusoidal frequencies in the analysis frame, i.e., the instantaneous frequency fluctuates around \( f_k \). In other words, an orbital component behaves as a narrow-band signal, whose bandwidth is...
much smaller than the Nyquist frequency and most of the spectral energy is clustered around $f_k$. Assuming that the range of the overall frequency variation is known for a given orbital component – which is user defined in the present approach – the mean frequency is associated with the strongest peak in the FFT of the signal in the frame. Although such a simple FFT-based peak-picking algorithm approach might introduce certain bias in the $f_k$ estimate, it is readily compensated by the flexibility of the proposed signal model (Fernando et al., 2004).

### 2.3.3 Degree of polynomials – $P$

This parameter is responsible for capturing variations in the terms $A_k (z_n) \sin(\phi_k (z_n))$ and $A_k (z_n) \cos(\phi_k (z_n))$ in Eqs. (4) and (5), respectively. For certain proxy records (up to approximately 50 Ma) variations in the instantaneous amplitude might be inferred from the theoretical model of an orbital component (e.g., numerical models of Laskar et al., 2004, 2011). However, the instantaneous phase fluctuations are in general unknown beforehand – at best the total bandwidth of an orbital component might be known (Laurin et al., 2016). Accordingly, there is not an analytical way to determine $P$ and once again it is necessary to resort to heuristics.

What is known is that the relationship $N–P$ is not arbitrary; broadly speaking, there is a direct dependence in the sense that larger $N$ requires larger $P$ and vice versa (McAulay and Quatieri, 1986). The reason is that smaller $N$ imposes a quasi-stationarity constraint on the signal – an orbital component behaves almost as a stationary sinusoid with only slightly changing instantaneous amplitude and frequency. In accordance, first-order polynomial approximation $P = 1$ is usually enough to properly address the modeling requirements in Eq. (9). Larger $N$ implies possibly stronger variations of the underlying sinusoids – the quasi-stationarity assumption has to be dropped and thus larger $P$ is needed. Bearing in mind the aforementioned discussion on the size of analysis frame, $P \in [1–3]$ is a reasonable choice for most proxy signals.

### 2.4 Uncertainty analysis

Providing reliable uncertainty bounds in this estimation approach is challenging. Our model is obtained by a weighted least-squares procedure, resulting at the same time in the estimated parameter values and an estimate of the covariance matrix. However, the covariance matrix is only valid if (i) there are no model errors or (ii) there is no exogenous noise in the system that is also passing through a nonlinear operation. Both elements are shortly discussed below.

Model errors: it is hard to avoid model errors on geological data. These model errors come from the polynomial approximations Eqs. (6)–(7). Accordingly, larger uncertainties (in this study expressed as standard deviations) are due to a low signal-to-noise ratio and/or fast instantaneous amplitude/frequency changes in the analysis frame. It turns out that model errors will increase the uncertainty on the estimates. There are two reasons for that: the model errors will increase the level of the residuals, and the residuals are no longer independent of the input (actually, they are uncorrelated).

Noise passing through the nonlinearity: if the disturbing noise is passing through the nonlinearity, the observed noise disturbances at the output of the system are no longer independent of the input. In that case all the classical methods to generate uncertainty bounds fail because these assume explicitly that the disturbing noise is independent of the input. In that case alternatives need to be developed to provide reliable uncertainty bounds, but to the best knowledge of the authors, such methods are not available yet. For that reason, the covariance matrix obtained from the estimation can be used as a first indication, but it should be used with care.

To provide a measure of uncertainty in this study, we use Monte Carlo simulations (using the covariance matrix) on the instantaneous frequency and sedimentation rate estimates. This was done through the following steps. Primary, it is assumed that the model parameters (polynomial coefficients) are normally distributed correlated random variables characterized by a $2K(P + 1)$ multivariate normal distribution.

Together with the model parameter estimates $\hat{\theta}$ in an analysis frame Eq. (A5), the MATLAB® least-squares routine “lscov” also returns the $2K(P + 1) \times 2K(P + 1)$ symmetric positive semi-definite covariance matrix $S$. This matrix contains the parameter variances on its diagonal; the rest of the elements are parameter covariance’s, which accounts for the correlation between the parameters.

By means of the MATLAB® routine “normrnd”, a set of random parameters entries were generated by sampling the multivariate normal distribution characterized by $\hat{\theta}$ and $S$.

With these entries the procedure (Eqs. 10–15) was carried out and the instantaneous frequency and sedimentation rate estimates in the analysis frame were obtained.

Steps (1)–(3) were run for all the analysis frames along the data record and the estimates were recomputed by means of the overlap–add strategy.

Steps (1)–(4) were run 100 times and the depth-variant standard deviations on the instantaneous frequency and sedimentation rate were obtained. The figures in this manuscript and the provided MATLAB® routines in the Supplement report by default 1 standard deviation ($1\sigma$).

The outcome of this process provides a hint on the size of the estimate uncertainties and equally on the spatial distribution of the uncertainty. As explained above, attention has to be payed to the absolute size of the uncertainties. Intervals in the analyzed record where the estimations are less reliable will be visible as peaks in the uncertainties, which is valuable information for interpreting and comparing the results of the analysis as a whole. Also the loss in power of an orbital period compared to the noise level causes peaks in uncertainty. This is because the ACE v.1 model always estimates a signal
in every analysis frame, even though the power of a signal does not stand out from the noise level.

3 Results and discussion

3.1 Synthetic insolation signal

To illustrate the proposed ACE v.1 model, a case study is presented on a modified insolation signal. As we are dealing with a synthetic case study aiming to introduce the mechanisms of the ACE v.1 model, we do not yet implement the uncertainty analysis. The basis of the analyzed signal is the classical 65° N summer (21 June) insolation curve (Milankovitch, 1941) for the last 6 Myr, as modeled by Laskar et al. (2004) (Fig. 2a). The periodogram shows the different obliquity and precession-related frequencies, which are the components determining the changes in insolation (Fig. 2b).

Subsequently, white and red noise are added to the original signal and made the conversion from the time domain towards the distance domain mimicking a changing sedimentation rate (SR) (Fig. 1c). The white noise is normally distributed (Gaussian) with the standard deviation providing the signal-to-noise ratio of 0.09. The red noise is generated as a first-order autoregressive process with the correlation factor equal to 0.999 giving rise to the signal-to-noise ratio of 0.003. To mimic a changing sedimentation rate, the time series is converted into distance series. The original time series has one sample 1 kyr\(^{-1}\). Initially, a constant SR of 2 cm kyr\(^{-1}\) is assumed to make a first conversion to the depth domain. The artificial changing SR is constructed by using the second degree polynomial shown in Fig. 2h–i. In practice, the input signal is interpolated, which increases the sampling rate much above the Nyquist frequency; next, the signal is resampled over the grid established by the SR.

The periodogram of the detrended signal is given in Fig. 2d, while its spectrogram is depicted in Fig. 2e. The level of white noise in combination with the changing SR has made the identification of the main ∼41 kyr obliquity (∼1.2 cycle m\(^{-1}\)) peak less obvious. The precession-related frequencies (∼2–2.8 cycle m\(^{-1}\)) are still clearly present; however, the merging of the ∼22 and ∼24 kyr periods into a single ∼23 kyr precession component and the resulting amplitude modulation must be noticed (Fig. 2e). The high-power peak around the 0.2 cycle m\(^{-1}\) frequency is the result of the introduced red noise.

With the user’s a priori knowledge, certain frequencies ranges – bandwidths – in the distance domain are interpreted as to correspond with the astronomical frequencies of obliquity and precession: ∼41 kyr obliquity [0.62–1.38] cycle m\(^{-1}\), ∼22 and 24 kyr precession [1.49–2.35] cycle m\(^{-1}\) and ∼19 kyr precession [1.75–2.75] cycle m\(^{-1}\). It must be pointed out that the model does not deal with the identification of the (orbital) components but that the components waveforms are simulated. The orbital component identification remains with the operator. In this particular case, the precession bandwidths overlap as a consequence of the distortion introduced by the artificial SR. As the characterization of this specific distortion is known by the users, the overlap for this case study could be dealt with separately by letting the bandwidths evolve along the record in function of the defined polynomial related to the SR change. However, in case a similar argumentation cannot be ensured for a case study, the use of the model in its current form is not recommended.

Providing these frequency ranges for this case study and a frame size of 5 m, the model estimates the three given components (Fig. 2f). As described in previous section, the choice of the frame size is a heuristic trade-off between (1) having at least some periods of your lowest frequency component in one frame and (2) being long enough to be able to separate closely spaced components. In this case, the obliquity period of 41 kyr [∼1.15 cycle m\(^{-1}\)] is considered as the lowest frequency to be taken into account. The aim is not to separate the ∼22 and ∼24 kyr precession components, but distinguish the merged ∼23 and the single ∼19 kyr periods.

From the modeled waveforms, the estimated instantaneous frequencies are extracted (Fig. 2g). To avoid potential discontinuities at the frame edges, the well-known overlap–add method is used (e.g., Verhelst, 2000). Essentially, overlapping data are summed and afterwards normalized again by a given weight, which is a function of the number of frame overlaps for a data point.

Using the a priori knowledge, the frequencies can be converted into SR estimates (Fig. 2h). Taking the average SR of all three modeled components (Fig. 2i), the distance series can be transposed into a time series. The periodogram of the new time series still contains traces of the white and red noise but is much cleaner than the modified insolation signal (Fig. 2j).

In summary, it is the user who needs to identify and provide a bandwidth for each component that is to be modeled and the size of the analysis frame. The selected bandwidths are typically based on other available geological constraints, such as bio- or magnetostratigraphy. This artificial case study illustrates the good performance of the model in estimating components, extracting the instantaneous frequencies and making a successful conversion towards the time domain. This conversion has been done autonomously by the algorithm for given frequencies that have to be traced. No band-pass-filtering or tuning to another form of model has been used. Here, the test started from a time series of insolation with very well-constrained orbital components. The following two case-studies deal with real geological case-studies.

3.2 ODP 846 benthic δ\(^{18}\)O record

The stratigraphy and chronology of the Pliocene–Pleistocene has benefited largely from benthic oxygen isotope records and its stacks (Lisiecki and Raymo, 2005; Huybers, 2007;
Figure 2. ACE v.1 analysis for a synthetic insolation signal. (a) 6 Ma insolation for 65° N 21 June (W m\(^{-2}\)) (Laskar et al., 2004). (b) The periodogram of the clean insolation signal as plotted in Fig. 2a. (c) To make the conversion from the distance towards the time domain a constant sedimentation rate of 2 cm kyr\(^{-1}\) is used. Using linear interpolation a non-constant sedimentation rate is mimicked. The changing sedimentation rates are plotted in Fig. 2h–i. Additional white and red noise are added to the signal as discussed in the text. (d) The periodogram of the modified insolation signal as plotted in Fig. 2c, which is noisier than the original periodogram (Fig. 2b) because of the added perturbations. (e) The spectrogram of the modified insolation signal. (f) The spectrogram of the three modeled components (41 kyr obliquity, 23 kyr precession and 19 kyr precession) using ACE v.1. (g) Estimated instantaneous frequencies for the three modeled components. (h) Using the associated astronomical periods of the modeled frequencies, the corresponding sedimentation rate is calculated and compared with the initial input change in sedimentation rate. (i) Comparison between the initial input change in sedimentation rate and the mean of the modeled components. (j) Periodogram of time series of the signal where the mean sedimentation rate estimate is used to make the conversion to the time domain.
Hilgen et al., 2012). One of the longest and most detailed records of this sort comes from ODP Site 846 from the tropical Pacific Ocean (3°06′S, 90°49′W; Mix et al., 1995; Shackleton et al., 1995). The length of the core is ~206 m, spanning the last 5.3 Myr and is sampled for benthic δ18O with an average resolution of 10 cm (~2.5 kyr; Mix et al., 1995; Shackleton et al., 1995). Spectral analysis has identified strong ~100 and ~41 kyr periodicities. While the origin of the 100 kyr cycle in the Pleistocene glacial is the subject of debate (Imbrie et al., 1993; Muller and MacDonald, 1997; Lisiecki, 2010), the 41 kyr periodicity can be attributed to obliquity. Other studies on ODP 846 alkenone-derived sea surface temperatures have shed light on the relative importance of obliquity and precession (high and low latitude) on the climatology of the tropical ocean system (Liu et al., 2004; Cleaveland and Herbert, 2007; Herbert et al., 2010). The ODP 846 benthic δ18O record is used in the reference LR04 Pliocene–Pleistocene benthic stack (Lisiecki and Raymo, 2005).

This record is selected for a case study as it is well studied and has an astronomically calibrated age model (LR04), which allows for the evaluation of the proposed approach. The raw data are the benthic δ18O depth series (Fig. 3a). After detrending, the periodogram and spectrogram reveal elevated spectral power around ~0.3 and ~0.6 cycle m⁻¹ (Fig. 3b, 3c). Using the a priori knowledge of the core, the first dominant frequency is identified as corresponding with a 100 kyr periodicity, while the ~0.6 cycle m⁻¹ corresponds with the 41 kyr obliquity. Figure 3d shows the spectrogram of the two modeled components. Following a similar reasoning as in the previous case study, an analysis frame size of 10 m is utilized. Using the instantaneous frequency estimates (Fig. 3e), the corresponding evolution of the sedimentation rate can be estimated (Fig. 3f). As the origin of the 100 kyr cycle is debatable (Imbrie et al., 1993; Muller and MacDonald, 1997; Lisiecki, 2010), the 41 kyr derived sedimentation rate is selected and compared with the SR as derived from the LR04 age model for the ODP 846 core (Fig. 3i). To do so, the stratigraphic levels are subtracted of subsequent samples and divided by their age (LR04) difference (Fig. 3i). This simple operation results in abrupt changes in sedimentation rate, which cannot be captured by the ACE v.1 model approach. These abrupt changes originate from the principle that the LR04 age model is based on a stack, which enhances the signal-to-noise ratio compared to an analysis on a single core. Moreover, it is tuned to an ice model that is driven by the 21 June insolation at 65° N. Therefore, in this study a 500-point running average is taken to smooth the results (Fig. 3i). Only the long-term-averaged trends are captured by our ACE v.1 estimation approach and not the fine-scaled sedimentation rates of the original LR04 age model. This is because (i) the ACE v.1 model in its current form cannot deal with fast changes in sedimentation rate, (ii) the signal-to-noise ratio of the stacked LR04 age model is superior to the ratio of a single record and (iii) no other a priori information, other than that the obliquity band should be in a certain frequency range, is used in the ACE v.1 analysis, contrary to the LR04 age model where other geological constraints are included. In the described approach, a frequency range is selected, which with the user’s a priori knowledge could be associated with the 41 kyr obliquity [0.47–0.71] cycle m⁻¹ and let the algorithms extract its waveform. The corresponding age model is then created by using the estimated instantaneous frequency changes and the association with the 41 kyr obliquity period.

Except for a small difference between 60 and 90 m the match between the results of the ACE v.1 model and the averaged LR04 age model is close. Remarkably, the interval has a pronounced elevated uncertainty on its estimation (Fig. 3g and h). The origin of the mismatch is the lower signal amplitude in this interval. Note the elevated signal amplitude is 70–80 m around the frequency of 0.5 cycle m⁻¹, whereas the 41 kyr component is mainly around the 0.6 cycle m⁻¹ (Fig. 3c). This feature in the ACE v.1 model suggests a small drop in sedimentation rate between 70 and 80 m (Fig. 3i), whereas the LR04 age model suggests a gradual rise in sedimentation rate in this interval. This mismatch could be reduced by increasing the lower boundary of the selected frequency range for the obliquity component estimation. A similar feature on a smaller scale is detectable around level 40–50 m (Fig. 3g). Between 140 m and the bottom of the core, there is low power in the 41 kyr frequency range. However, in contrast to the 60–90 m interval, there are no neighboring (in the frequency domain) elevated signal amplitudes. The loss of power in this frequency range at this position translates into an elevation of the uncertainty on the estimations for this interval (Fig. 3g and 3h). In general, the comparison between the ACE v.1 modeled sedimentation rates and LR04 sedimentation rates yields satisfactory results, as stratigraphic intervals where a mismatch exists are red-flagged by increased uncertainty on the ACE v.1 model. The sign of the mismatch in sedimentation rates is not consistent throughout the core, which means that over- and underestimates of sedimentation rates cancel each other out. In this particular case study, there seems to be an overestimation in total duration (compared to the LR04 age model) of ~5%, which is significant but not so bad, considering that we simply used the tracking of the obliquity-related frequency. The periodogram of the tuned record, based on the 41 kyr derived SR, reveals a much cleaner signal (Fig. 3j). Using the comparison between the SR derived in this novel approach and deduced from the LR04 age model for the ODP 846 record (Fig. 3i), the conclusion is that again the algorithm performs well in capturing the main-averaged trend.

3.3 Danian magnetic susceptibility record

This second case study is related to a Danian magnetic susceptibility (MS) record from the pelagic carbonate C tessica Highway section, Gubbio, Italy. The Gubbio sections are well-known for their pioneering studies including plank-
Figure 3. ACE v.1 analysis for a Pliocene–Pleistocene benthic oxygen isotope record. (a) ODP Site 846 \( \delta^{18}O \) record (W m\(^{-2} \)) (Mix et al., 1995; Shackleton et al., 1995). (b) The periodogram of the ODP Site 846 \( \delta^{18}O \) record as plotted in Fig. 2a. (c) The spectrogram of the ODP Site 846 \( \delta^{18}O \) record. (d) The spectrogram of the two modeled components (100 kyr periodicity and 41 kyr obliquity) using ACE v.1. (e) Estimated instantaneous frequencies for the two modeled components. (f) Using the associated (astronomical) periods of the modeled frequencies, the corresponding sedimentation rate is calculated. (g) The uncertainties on the estimated instantaneous frequencies (1\( \sigma \)). (h) The uncertainties on the sedimentation rate estimates (1\( \sigma \)). (i) Comparison between the ACE v.1 estimated sedimentation rate and the derived non-averaged and 500-point-averaged sedimentation rates for ODP Site 846 according to the age model of the LR04 stack (Lisiecki and Raymo, 2005) and the estimated change in sedimentation rate based on the modeled obliquity component. (j) Periodogram of time series of the signal where the mean sedimentation rate estimate is used to make the conversion to the time domain.
Because of tidal dissipation, the periodicity of obliquity cycles has been used as calculated by Berger et al. (1992). Accordingly, a duration of 39.6 kyr per obliquity cycle is estimated. Here, a duration of 39.6 kyr per obliquity cycle is estimated. The constraint of the use constant band-pass filter ranges for a (sub-)record disappears with the ACE v.1 modeling approach.

4 Conclusions and prospects

This study introduces a new approach to time-series analysis in the field of cyclostratigraphy. The main focus is on the estimation of already identified components in a signal. The identification (or detection) of the components is based on the a priori knowledge of the user, given available geological constraints. Those components are given a frequency range, which is determined by the user and can correspond with astronomical periods of, e.g., eccentricity, precession and obliquity. Once this first step has been taken, the selected components are simulated by making use of a model that is not based on FFT-derived methods, band-pass filtering or other commonly used methods in cyclostratigraphy but one that relies on polynomial modeling. Basic uncertainty analysis is provided too in order to be able to assess the size and distribution of the model estimate uncertainties.

The ACE v.1 model in its current version should be used under the following constraints: (1) significant sinusoidal-
Figure 4. ACE v.1 analysis for a Danian magnetic susceptibility record. (a) Contessa Highway Danian magnetic susceptibility record (m$^3$ kg$^{-1}$) (Sinnesael et al., 2016). (b) The periodogram of the Danian magnetic susceptibility as plotted in Fig. 2a. (c) The spectrogram of the Danian magnetic susceptibility record. (d) The spectrogram of the three modeled components (100 kyr eccentricity, 39.6 kyr obliquity and 22.5 kyr precession) using ACE v.1 (Berger et al., 1992). (e) Estimated instantaneous frequencies for the three modeled components. (f) Using the associated (astronomical) periods of the modeled frequencies, the corresponding sedimentation rate is calculated. (g) The uncertainties on the estimated instantaneous frequencies (1$\sigma$). (h) The uncertainties on the sedimentation rate estimates (1$\sigma$). (i) Periodogram of time series of the signal where the mean sedimentation rate estimate is used to make the conversion to the time domain. (j) Comparison between the ACE v.1 estimated sedimentation rates and the derived sedimentation rates in the studies by Galeotti et al. (2015) and Sinnesael et al. (2016).
like variations can be detected and identified in a proxy record, (2) the frequency ranges of the components cannot overlap for a given analysis, (3) the user makes an appropriate tradeoff between the analysis frame size and the degree of the used polynomials and (4) no fast changes in sedimentation rate can be detected.

The first case study on a controlled modified insolation signal document the ability of this proposed new approach to successfully model components of a signal. Furthermore, it shows that the estimated instantaneous frequencies derived from the modeling can easily be converted to sedimentation rates, which can be used to convert distance series into time series. A more robust result is obtained by taking the average sedimentation rate of the different estimated components. New spectral analysis shows strongly reduced levels of both white and red noise.

Also the second case study concerning the benthic $\delta^{18}O$ record of ODP Site 846 illustrated key features of the proposed ACE v.1 model. The tracking of the obliquity component is successful and the derived sedimentation rates on the basis of this modeled component are in close agreement with the average age model for ODP846 as constructed by LR04. However, only the long-term-averaged trends are captured and not the fine-scaled sedimentation rates of the original LR04 age model. This is because (a) the ACE v.1 model in its current form cannot deal with fast changes in sedimentation rate (b) the signal-to-noise ratio of the LR04 is superior to the ratio of a single record and (c) no other a priori information coming from other geological constraints is included as that the obliquity band should be in a certain frequency range. Moreover, the practical use of the uncertainty analysis on the size and distribution of the model estimates is well exemplified. This case study illustrates too that the suggested approach is an additional instrument in time-series analysis to automatically extract waveforms and derive time. As such one can exclude the human influence in the tuning process (often heuristically determining relative minima and maxima in a proxy record). However, the verification with available geological constraints remains essential in the validation of the model.

The third case study dealt with a Danian magnetic susceptibility record from the Contessa Highway section Gubbio, Italy. It forms a good illustration of how a priori knowledge is used to select certain components to model, but also how the results of the model can be coupled back to existing interpretations. Moreover, it demonstrates the disadvantages of using the classical band-pass-filtering approach in the tuning process, which is circumvented with this new modeling approach. The approach sheds new light on the astrochronological age model and derived sedimentation rates of the Danian in Gubbio. Following the model, there is probably no significant drop in SR in the oldest half of the Danian section in Gubbio, but there is a suggested increase in SR from the middle of magnetochron C27r. Again the crucial role of the verification of the model results with other available geological constraints must be emphasized, in this case as discussed in Galeotti et al. (2015) and Sinnesael et al. (2016).

This paper convincingly introduces the principles and illustrates the functioning of the concept of time-series analyses by polynomial modeling of sinusoidal behavior in Earth science proxy series. Further work will concentrate on (i) automated identification of significant components, (ii) the release of the constraint of non-overlapping of the component’s frequency ranges and (iii) allowing for the tracking of faster sedimentation rate changes. Note, that this modeling approach is designed to be used in a cyclostratigraphical framework. However, it can easily be adapted for all kind of time-series analyses on data, which contain significant cyclic (sinusoidal) variation. The reader is invited to make use of the ACE v.1 model and provide feedback on its functioning and further development.

5 Code availability

The ACE v.1 model is designed in MATLAB® and all scripts are available in the Supplement. These include a main script that enables the user to load data, define model parameters, use the functions and produce basic graphical output. Also the separate scripts of the three functions “OrbitalComponentEstimation”, “SedimentationRateEstimation” and “UncertaintyAnalysis” are included as well as an instructive manual “Manual_ACEv1_Model_Sinnesael_etal_2016_GMD.txt”.

6 Data availability

Data used for the ODP Site 846 case study are available on doi:10.1594/PANGAEA.696444 (Mix et al., 1995). Data used for the Danian magnetic susceptibility record are available on doi:10.1594/PANGAEA.864450 (Sinnesael et al., 2016).
Appendix A: Estimation of the model parameters

The model parameters in Eq. (8) are estimated by minimizing the following cost function in the matrix form in the least-squares sense:

$$\min (y - H\theta)^T (y - H\theta),$$  \hspace{1cm} (A1)

where the symbol $T$ denotes the matrix transpose operator. The elements in Eq. (A1) are defined as follows:

- Vector containing the stratigraphic data
  \[ y = (y(z_1), y(z_2), \ldots, y(z_N))^T, \]  \hspace{1cm} (A2)

- Vector containing the model parameters
  \[ \theta = (a_{1,0}, a_{1,1}, b_{1,0}, \ldots, a_{K,0}, a_{K,1}, b_{K,0}, \ldots, b_{K,P})^T, \]  \hspace{1cm} (A3)

- Matrix containing the signal model
  \[ H = (H_{1,s} H_{1,c} H_{2,s} H_{2,c} \cdots H_{K,s} H_{K,c}), \]  \hspace{1cm} (A4)

with

\[
H_{k,s} = \begin{pmatrix}
\sin(2\pi f_k z_1) & \sin(2\pi f_k z_1) & \cdots & \sin(2\pi f_k z_1) \\
\sin(2\pi f_k z_2) & \sin(2\pi f_k z_2) & \cdots & \sin(2\pi f_k z_2) \\
\vdots & \vdots & \ddots & \vdots \\
\sin(2\pi f_k z_N) & \sin(2\pi f_k z_N) & \cdots & \sin(2\pi f_k z_N)
\end{pmatrix},
\]

\[
H_{k,c} = \begin{pmatrix}
\cos(2\pi f_k z_1) & \cos(2\pi f_k z_1) & \cdots & \cos(2\pi f_k z_1) \\
\cos(2\pi f_k z_2) & \cos(2\pi f_k z_2) & \cdots & \cos(2\pi f_k z_2) \\
\vdots & \vdots & \ddots & \vdots \\
\cos(2\pi f_k z_N) & \cos(2\pi f_k z_N) & \cdots & \cos(2\pi f_k z_N)
\end{pmatrix}.
\]

The solution to the least-squares problem Eq. (A1) is the vector of sought model parameters:

$$\hat{\theta} = H^+ y,$$  \hspace{1cm} (A5)

where $H^+$ is the pseudo inverse of $H$. 

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